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Kobayashi et al.

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(54) **CONNECTING STRUCTURE FOR PRESSURE PIPING**

(76) Inventors: **Kazumi Kobayashi**, Fukuyama (JP);
Masato Kobayashi, Fukuyama (JP)

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F16L 23/024 (2006.01)

F16L 25/08 (2006.01)

(52) **U.S. Cl.**

CPC **F16L 21/00** (2013.01); **F16L 23/024**
(2013.01); **F16L 25/08** (2013.01)

(58) **Field of Classification Search**

USPC 285/417, 403, 404, 369, 371; 403/362,
403/306

See application file for complete search history.

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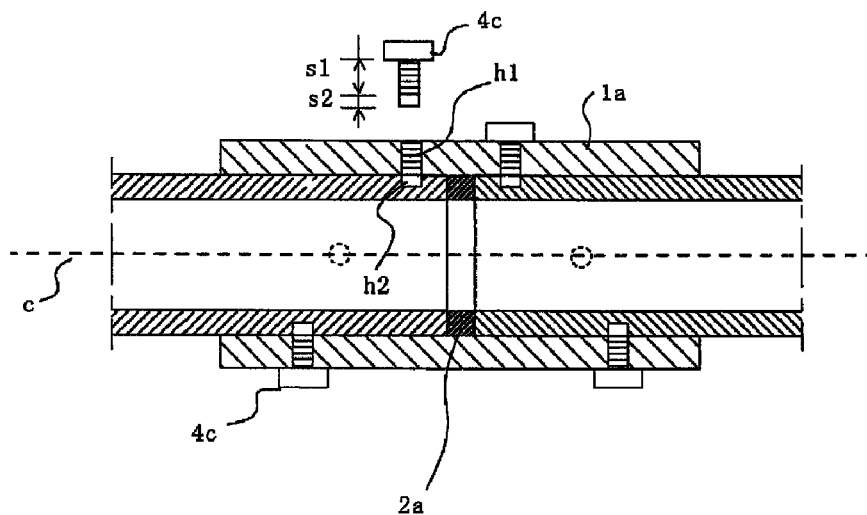
Primary Examiner — Aaron Dunwoody

(74) *Attorney, Agent, or Firm* — Merek, Blackmon & Voorhees, LLC

(57) **ABSTRACT**

in order to connect pressure pipes in a fluid-tight manner on-site without welding, a plurality of through holes (h1) are provided in a cylindrical sleeve (1a) at separate locations in the lengthwise direction, and with identical angular intervals around the circumference of the cylindrical sleeve without overlapping in the circumferential direction. Non-through holes (h2) in which screw threads have been formed are provided in pressure plates (P1, P2) at locations corresponding to the holes (h1). An insert (2a) has a pair of opposing annular faces (31, b2), and annular ring grooves (b11, b21) are formed respectively in the annular faces (b1, b2) to house O-rings (3). The insert (2a) is inserted into the sleeve (1a), after which the pressure pipes (P1, P2) are inserted, one from either side, into the interior of the sleeve (1a), and bolts (4) are inserted into the plurality of holes (h1) in the sleeve (1a), and screwed onto the screw threads of the pressure pipes (P1, P2).

3 Claims, 22 Drawing Sheets



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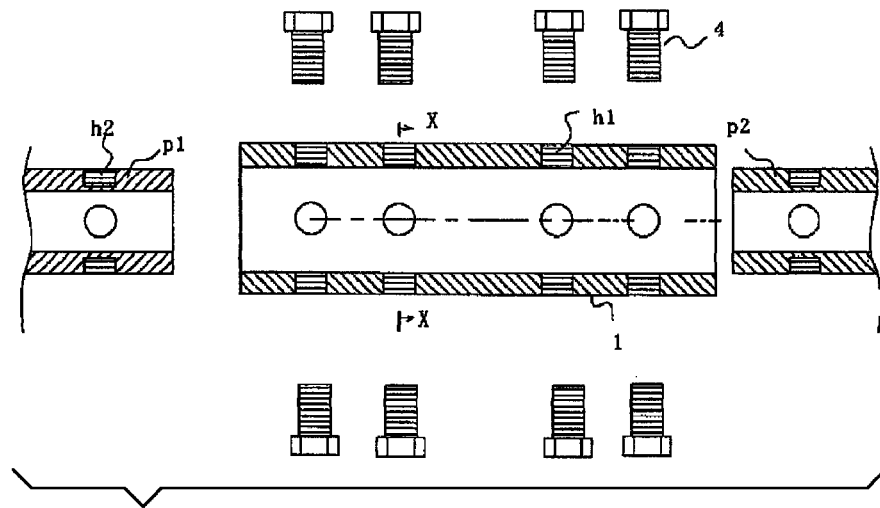


FIG. 1A

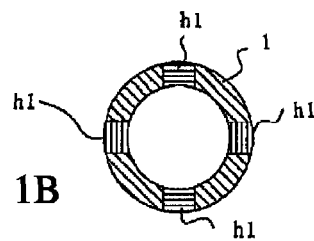


FIG. 1B

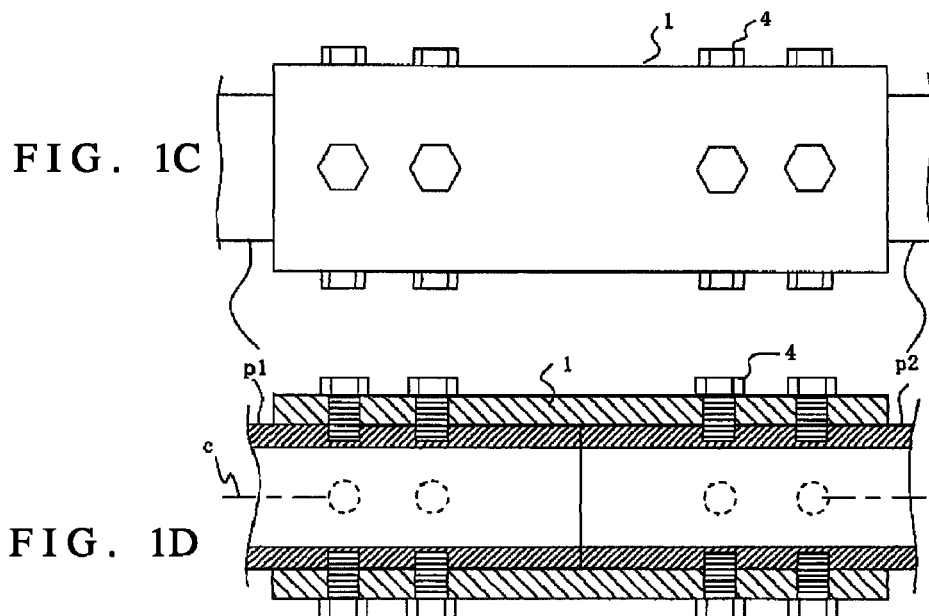


FIG. 1C

FIG. 1D

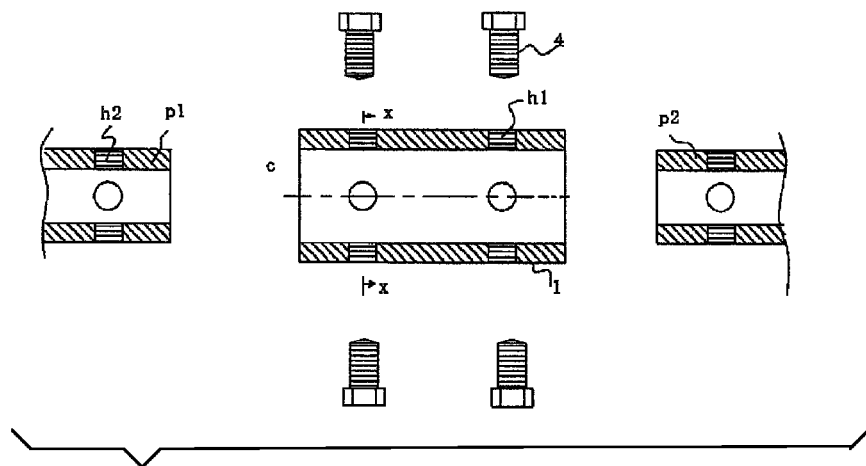


FIG. 2A

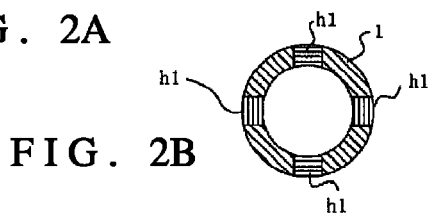


FIG. 2B

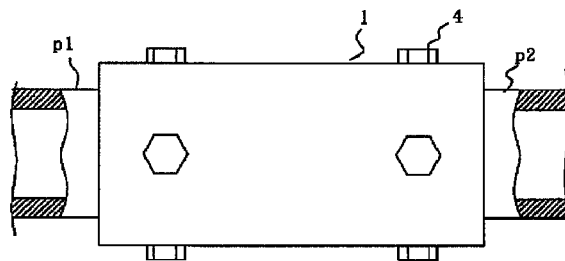


FIG. 2C

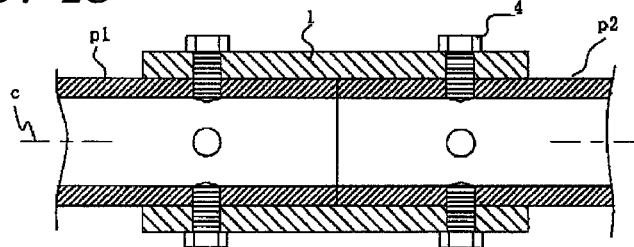


FIG. 2D

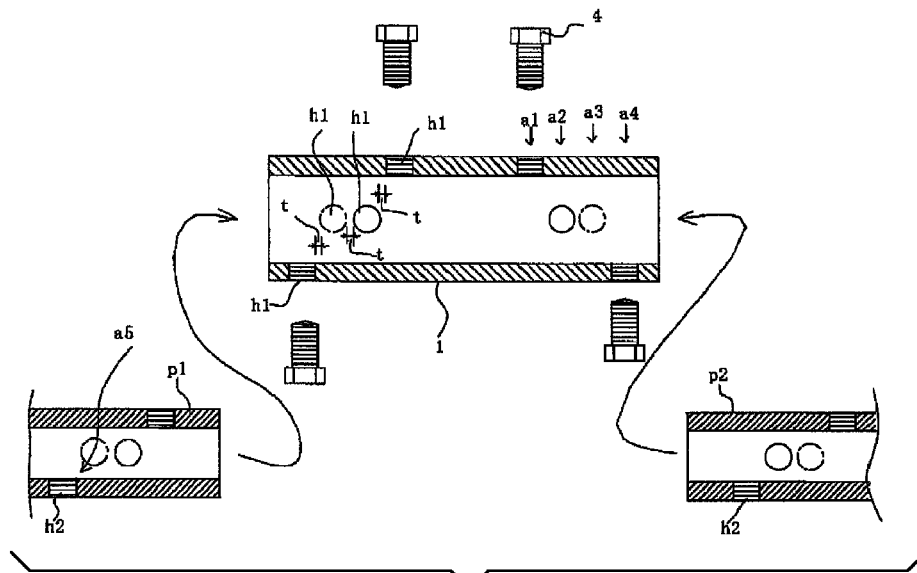


FIG. 3A

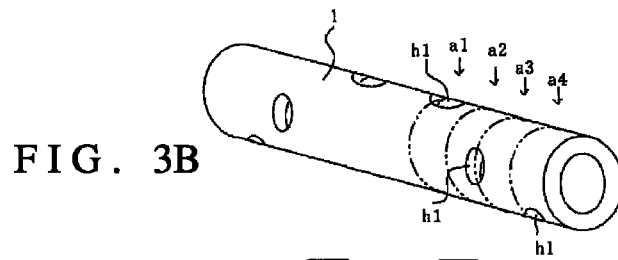


FIG. 3B

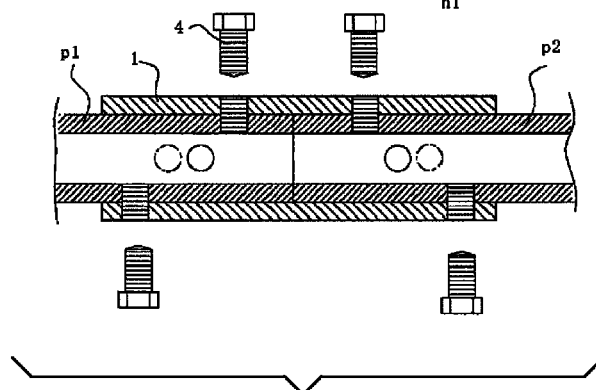


FIG. 3C

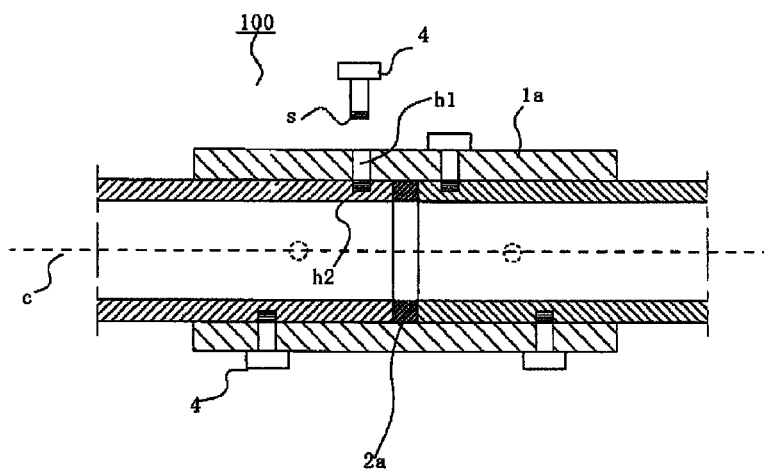


FIG. 4A

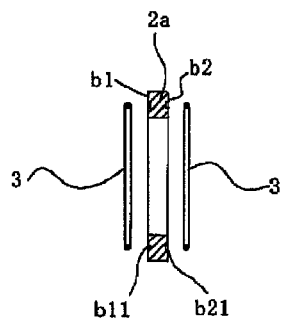


FIG. 4B

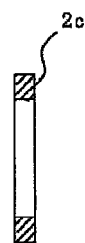


FIG. 4C

FIG. 5

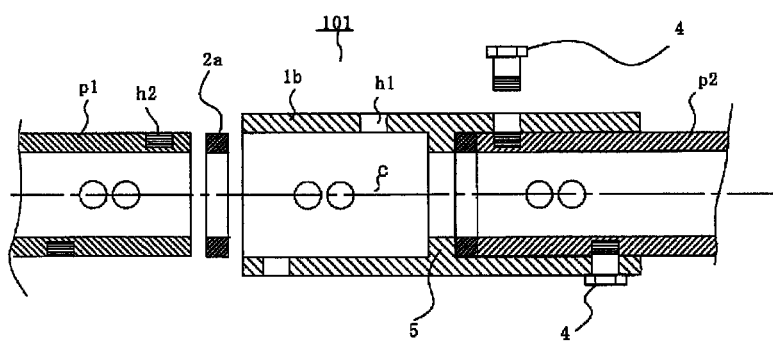
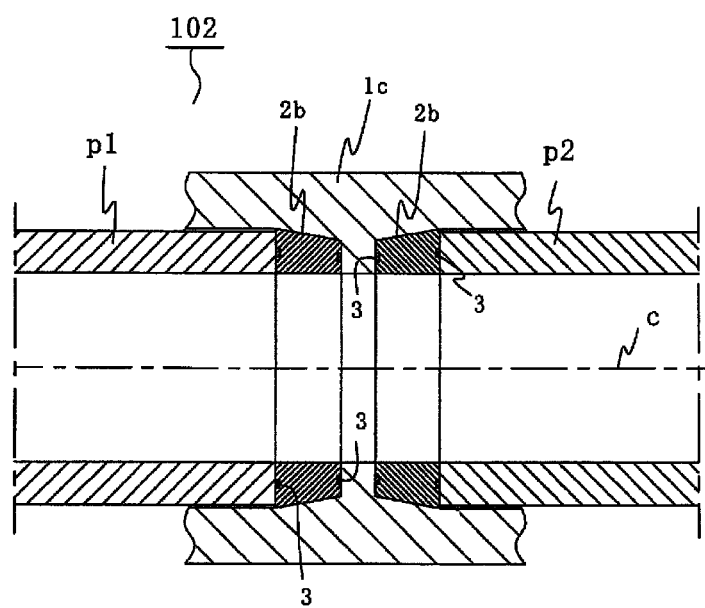


FIG. 6



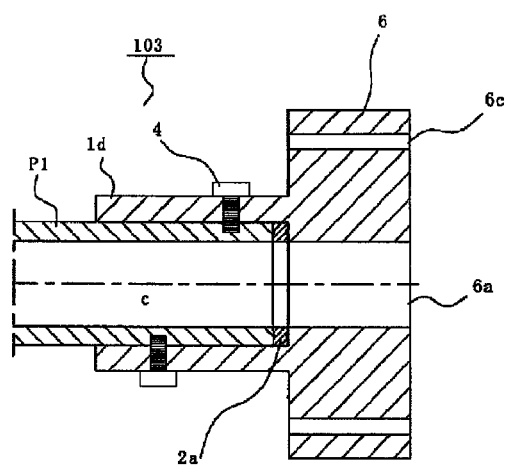


FIG. 7A

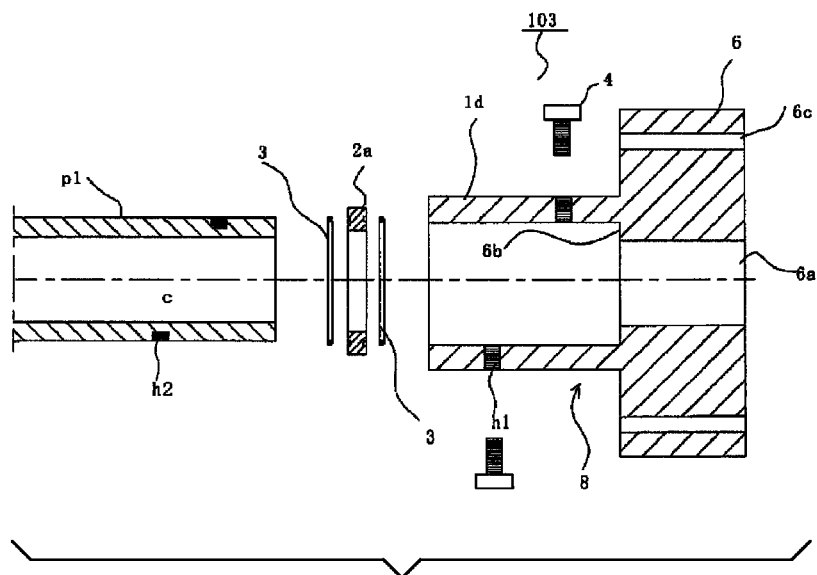


FIG. 7B

FIG. 8

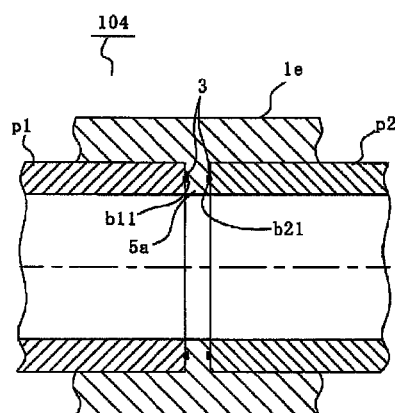


FIG. 9

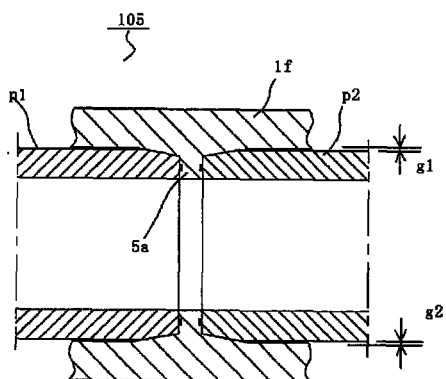


FIG. 10A

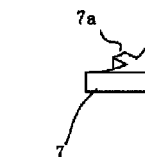
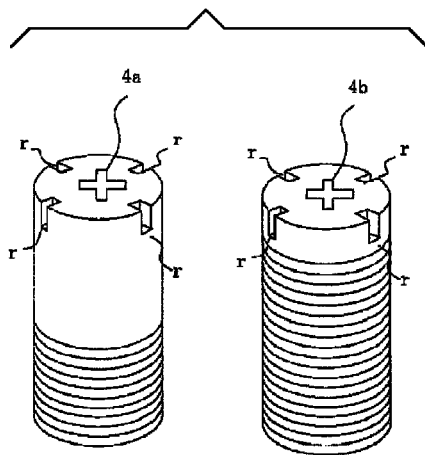


FIG. 10B

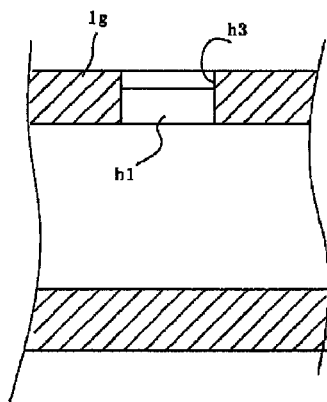


FIG. 10C

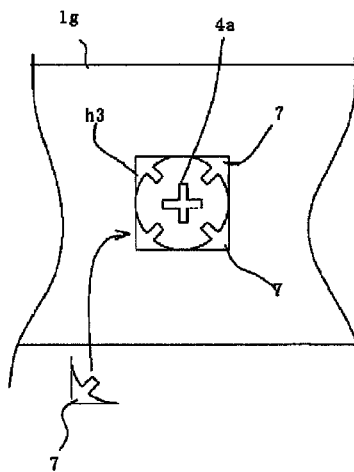


FIG. 10D

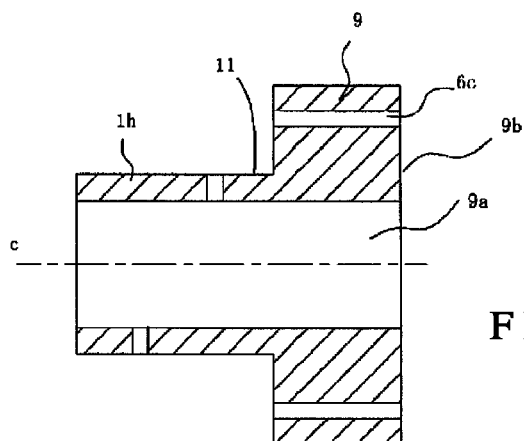


FIG. 11A

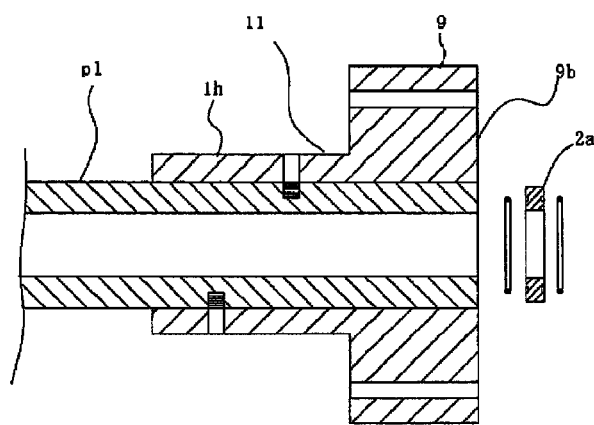
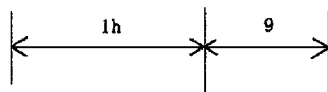


FIG. 11C

FIG. 11B

FIG. 12

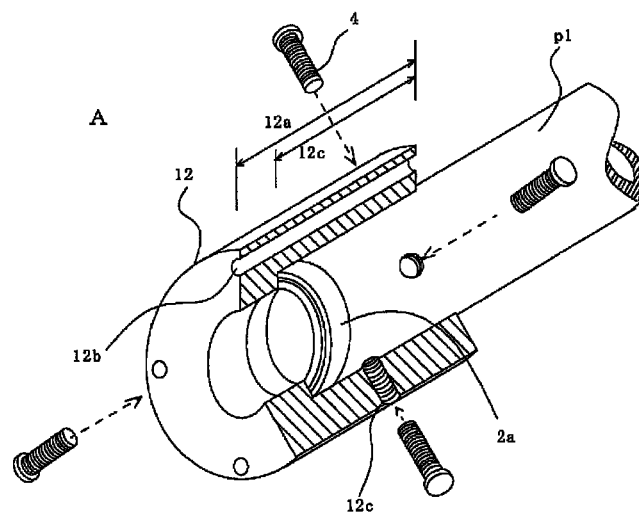
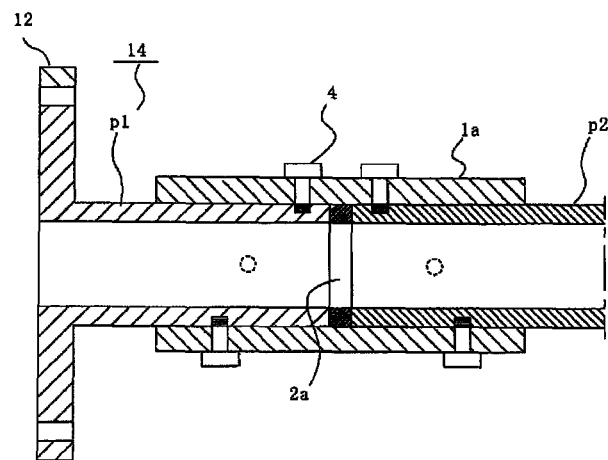


FIG. 13



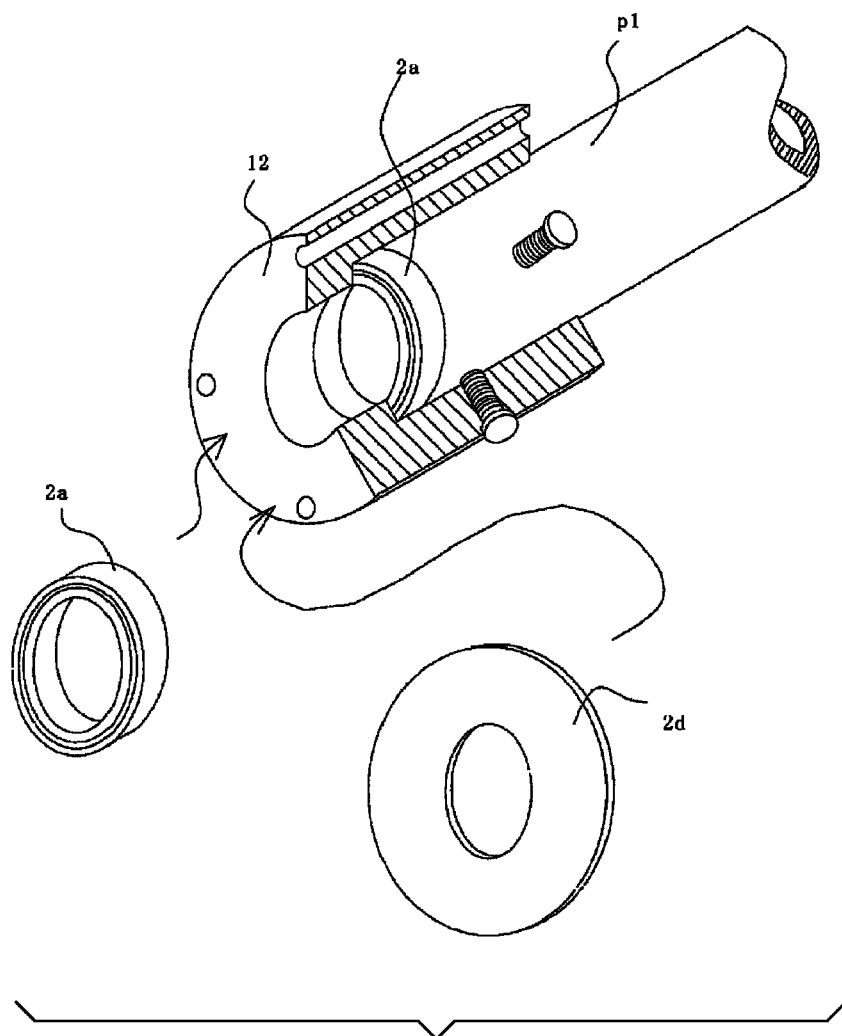


FIG. 14

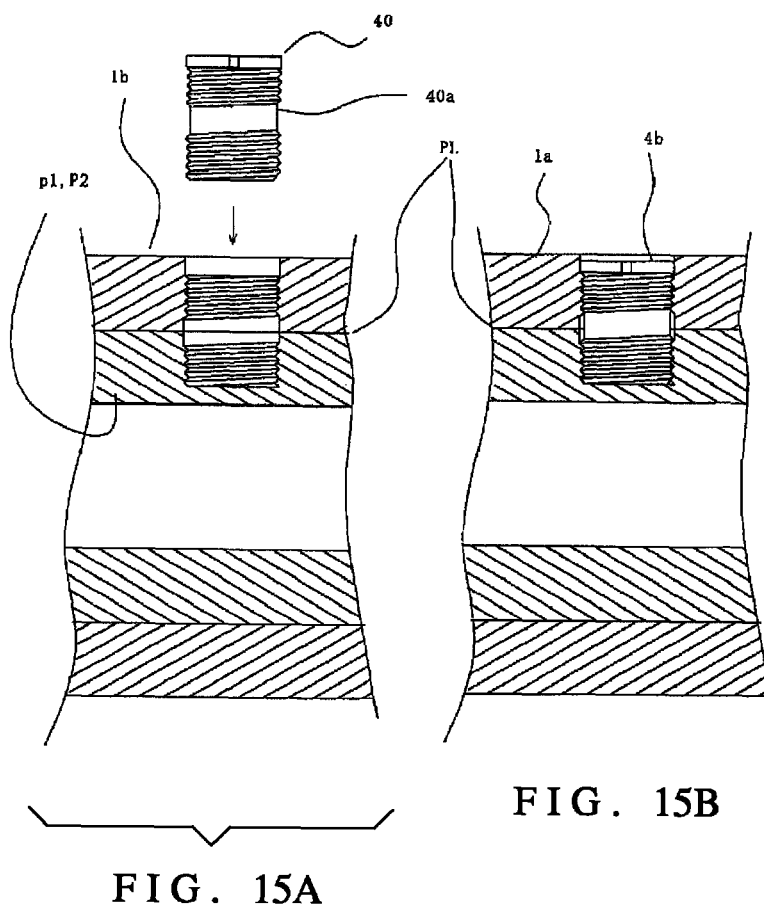
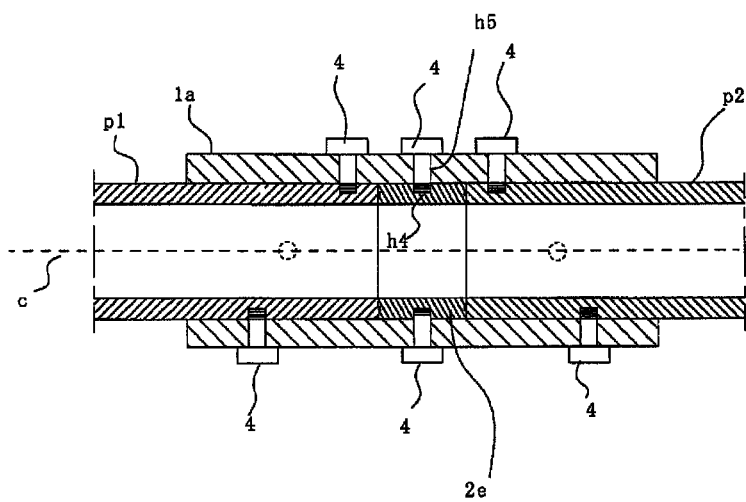


FIG. 16



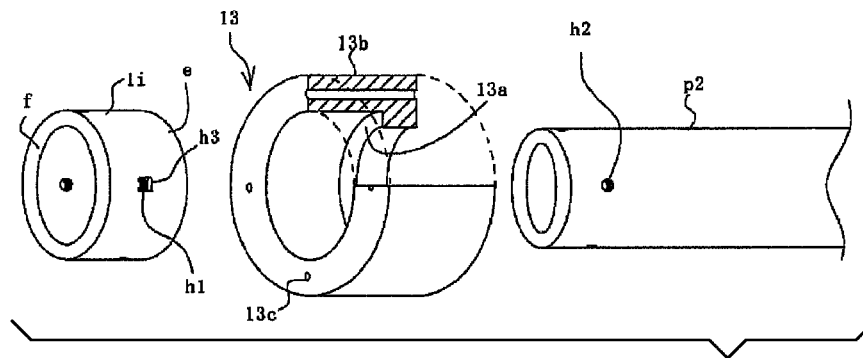


FIG. 17A

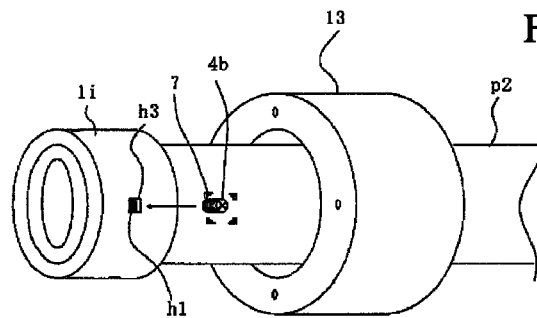


FIG. 17B

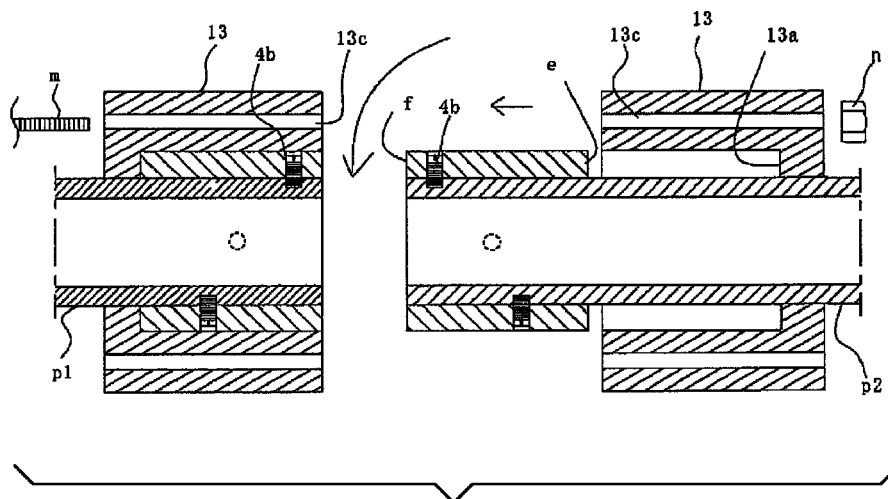


FIG. 17C

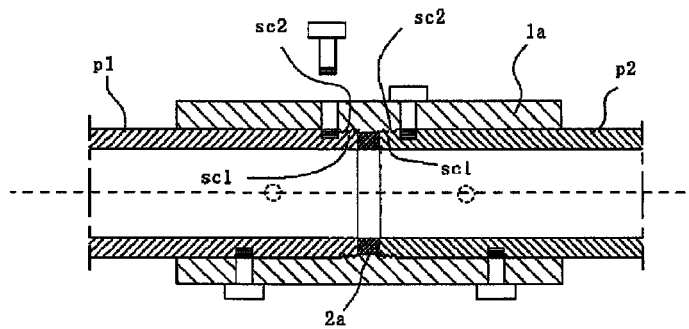


FIG. 18A

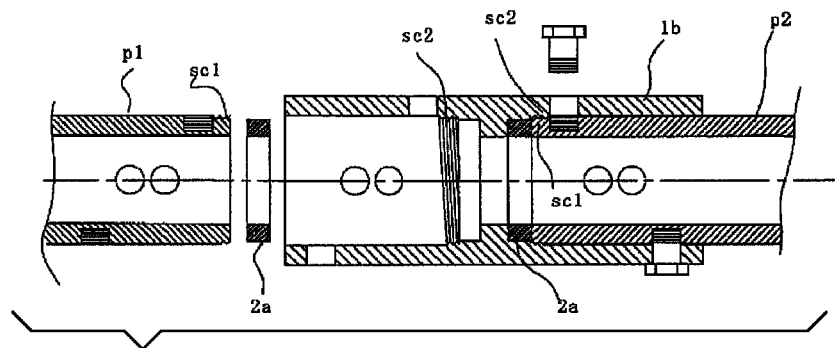


FIG. 18B

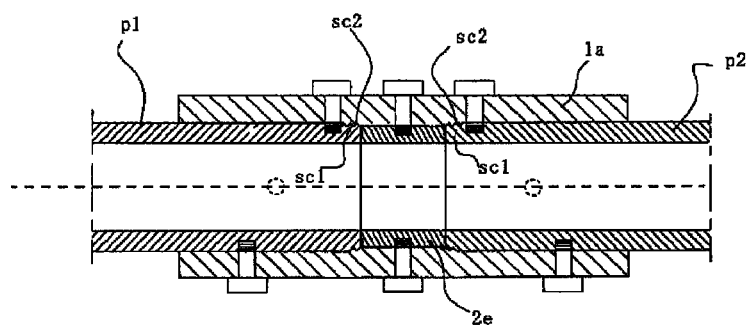
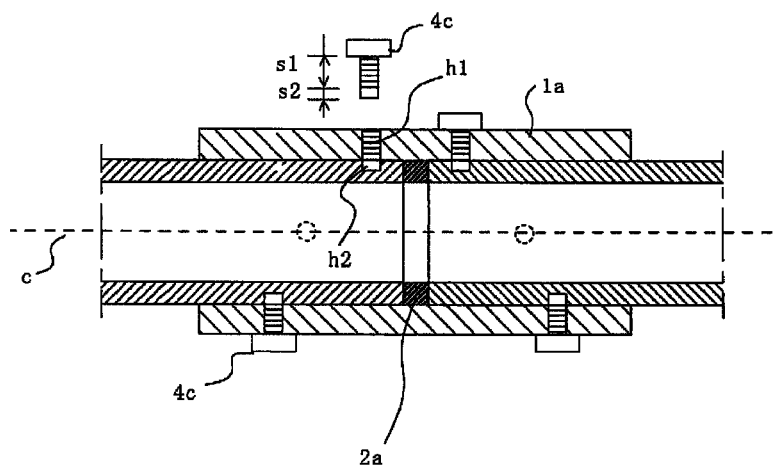


FIG. 18C

FIG. 19



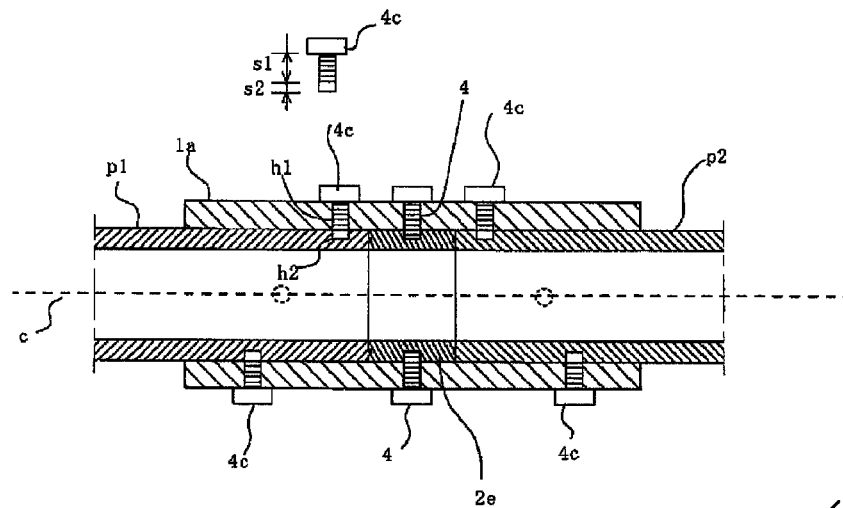


FIG. 20A

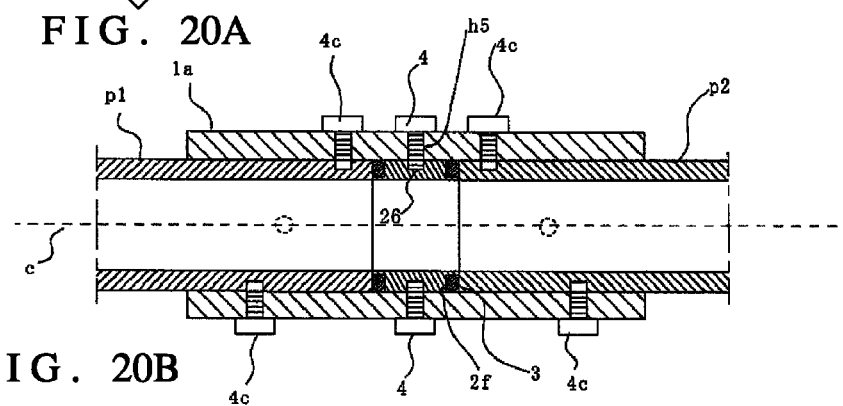


FIG. 20B

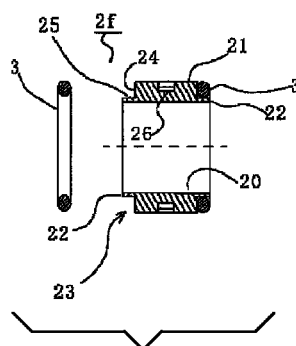


FIG. 20C

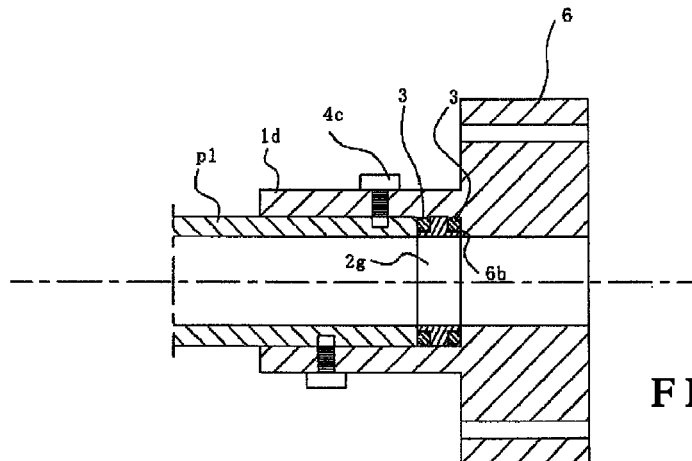


FIG. 21A

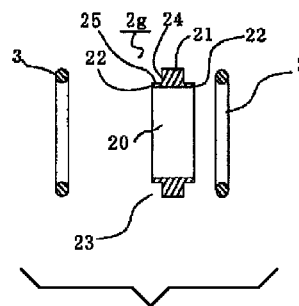


FIG. 21B

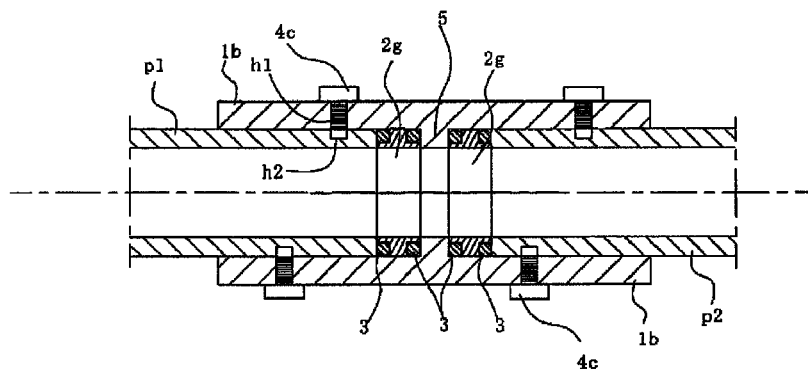


FIG. 21C

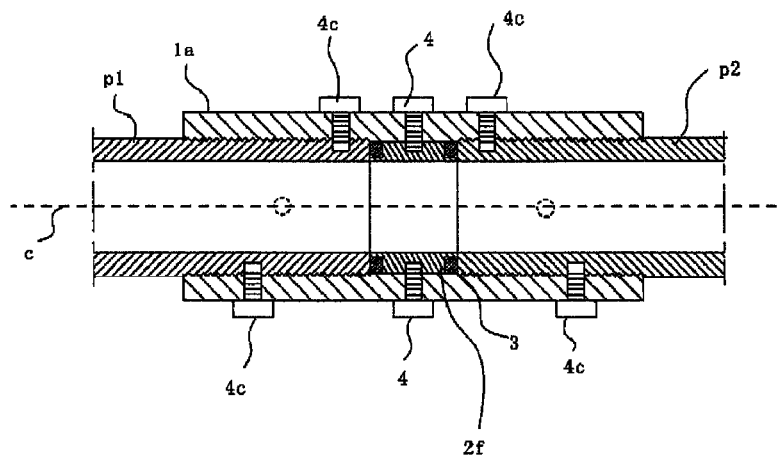


FIG. 22A

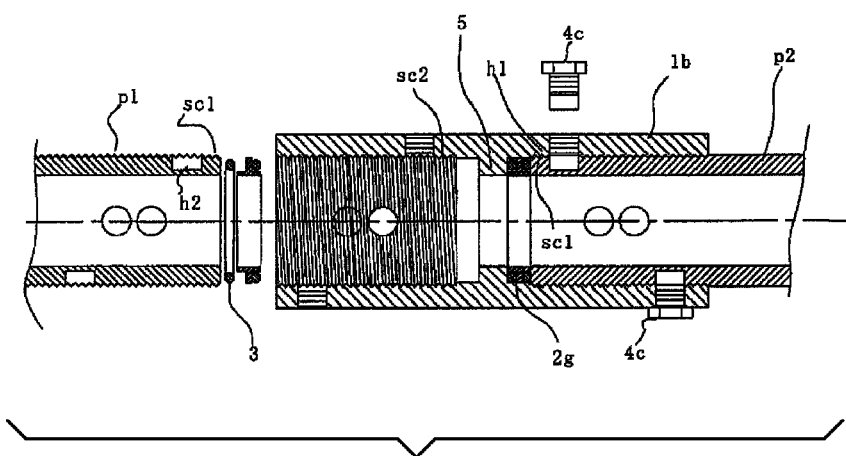


FIG. 22B

CONNECTING STRUCTURE FOR PRESSURE PIPING**CROSS-REFERENCE TO RELATED APPLICATION**

The present application claims the priority under 35 U.S.C. 119 of Japanese Application No. 2011-004969, filed Jan. 13, 2011, which is hereby incorporated herein by reference in its entirety.

TECHNICAL FIELD

The present invention relates to a connecting structure for pressure piping for permitting connection of the pressure piping on-site without requiring welding.

BACKGROUND ART

In Japanese Industrial Standards, the strength of couplings that should be used is defined for connected pressure piping. In particular, concerning the strength of couplings, the strength that the base material of the pressure piping connected to the coupling must have before failure in a tension test is defined. In addition, with respect to a connection by welding, the pressure piping is required to extend a leg length for all over the place in order to keep weld strength that the base material of the pressure piping before failure in the same way. Such welding work requires skill, and therefore, the number of persons able to perform the work is limited.

Different connecting means than welding includes adhesive and bolts. For example, patent literatures 1 and 2 disclose means for combining pipe and pipe by bolts. These technologies are to fix pipes for accommodating electric wires with the fastening force of bolts screwed on peripheral surface walls of the pipes in their radial direction. These pipes are to protect the inner electric wires, and the electric wires in themselves do not either have pressure or leak. Patent literature 3 discloses a technique for connecting poles with the bolts, wherein the poles are fixed with the fastening force of the bolts.

RELATED ART DOCUMENTS**Patent Documents**

Patent literature 1: Japanese Examined Utility Model Application Publication No. 51-9667

Patent literature 2: Japanese Unexamined Patent Application Publication No. 2003-180011

Patent literature 3: Japanese Unexamined Patent Application Publication No. 2010-180957

SUMMARY OF THE INVENTION**Object to be Solved by the Invention**

In connecting pressure piping for transmitting high pressure fluid without using welding, it is necessary to keep a high tensile strength to seal in the internal fluid. In the above-mentioned bolt-connecting, it is predicted that the connecting strength is improved by enhancing the material strength of the bolts, bolt diameter, and/or fastening pressure. However, a problem about an arrangement to improve the strength or a means to seal a fluid flowing through the pressure piping has

not been solved. The present invention aims to provide a connecting structure for pressure piping using bolts as a connecting means.

Means to Solve the Problem

The present invention is characterized by a connecting structure for connecting pressure piping to convey pressure fluid inside, including a cylindrical sleeve having a plurality of through holes at separate locations in a lengthwise direction, and with identical angular intervals in the circumferential direction and without overlapping in the circumferential direction, and a plurality of bolts to be inserted into the through holes of the sleeve. Non-through holes having screw threads are provided in the pressure piping at locations corresponding to the holes of the sleeve. When the pressure piping is inserted into the interior space of the sleeve, the non-through holes of the pipes open into the through holes of the sleeve, and the bolts are screwed into the communicating holes.

Effects of the Invention

According to pipe couplings of the present invention, it is possible to connect the pressure piping with the bolts without using welding in furnishing the pressure piping in which the tensile strength is required.

BRIEF DESCRIPTION OF THE DRAWINGS

FIGS. 1A, 1B, 1C and 1D illustrate a test sample of a connecting structure.

FIGS. 2A, 2B, 2C and 2D illustrate another test sample of a connecting structure.

FIGS. 3A, 3B and 3C illustrate yet another test sample of a connecting structure.

FIGS. 4A and 4B illustrate a connecting structure according to a first embodiment. FIG. 4C illustrates an alternative form of insert.

FIG. 5 illustrates a connecting structure according to a second embodiment.

FIG. 6 illustrates a connecting structure according to a third embodiment.

FIGS. 7A and 7B illustrate a connecting structure according to a fourth embodiment.

FIG. 8 illustrates a connecting structure according to a fifth embodiment.

FIG. 9 illustrates a connecting structure according to a sixth embodiment.

FIGS. 10A, 10B, 10C and 10D illustrate a connecting structure using a detent according to a seventh embodiment.

FIGS. 11A, 11B and 11C illustrate a connecting structure according to an eighth embodiment.

FIG. 12 illustrates a connecting structure according to a ninth embodiment.

FIG. 13 illustrates a connecting structure according to a tenth embodiment.

FIG. 14 illustrates a connecting structure according to an eleventh embodiment.

FIGS. 15A and 15B illustrate a connecting structure according to a twelfth embodiment.

FIG. 16 illustrates a connecting structure according to a thirteenth embodiment.

FIGS. 17A, 17B and 17C illustrate a connecting structure according to a fourteenth embodiment.

FIGS. 18A, 18B and 18C illustrate a connecting structure according to a fifteenth sixteenth embodiment.

FIG. 19 illustrates a connecting structure according to a sixteenth embodiment.

FIGS. 20A, 20B and 20C illustrate connecting structures according to seventeenth and eighteenth embodiments.

FIGS. 21A, 21B and 21C illustrate connecting structures according to nineteenth and twentieth embodiments.

FIGS. 22A and 22B illustrate a connecting structure according to a twenty-first embodiment.

MODE FOR CARRYING OUT THE INVENTION

The tensile strength of a connecting structure for connecting pressure piping with bolts will be examined. In the above-mentioned patent documents, pipes are connected by transformation of the outer circumferential walls of the pipes, which is caused by the pressing force of screwed bolts. On the other hand, in a pressure piping equipment, the tensile strength for the pressure piping is set forth in the Japanese Industrial Standards, and to obtain enough connecting force, the bolts are inserted into holes provided on the pressure piping in addition to the transformation of the outer circumferential walls.

Besides, although the breaking strength of the pressure piping itself decreases because the holes are provided on the pressure piping, an object of the present embodiment is to obtain a connecting strength that is greater than the yield load of the pressure piping.

FIG. 1 is a view for explaining a sample used in a test. The sample according to FIG. 1 is so constructed that pressure pipes p1, p2 are inserted from both sides of a cylindrical sleeve 1 and screwed with four bolts extending through holes h1, h2 through the sleeve 1 at 90° intervals on the same circle, that is, along the same plane transverse to the longitudinal axis of the cylindrical sleeve, to connect the cylindrical sleeve to the pressure pipes p1, p2. FIG. 1B is a cross-sectional view of FIG. 2 taken along the line X-X, showing the situation in which the holes h1 are drilled through the sleeve 1 at 90 degree intervals. FIG. 1C shows the situation in which the bolts 4 are screwed into the holes, and FIG. 1D is a cross-sectional view of FIG. 1C.

Even when the bolts 4 are tightened, an inner wall of the sleeve 1 does not equally adhere on outer walls of the pressure pipes p1, p2. A reason is that the walls of the cylindrical sleeve 1 and the pipes p1, p2 one side of the connecting structure move away from each other when the walls of the cylindrical sleeve 1 in the pipes p1, p2 on the other side are closely adhered by tightening the bolts 4. Accordingly, in the case of the connecting structure like this sample, the tensile strength of the connecting structure depends not on the frictional force of the walls by tightening of the bolts 4, but wholly on the ability of the bolts to withstand the shearing force at a gap between the sleeve and the pressure pipes due to the tensile force imposed by the pipes on the connecting structure.

First, concerning the sample of FIG. 1, the relation between the tensile strength and cross-sectional area of the bolt 4 is examined by using eight bolts having a strength smaller than the strength of the pressure pipes p1, p2. The pressure pipes p1, p2 are made of STPT410 (carbon steel pipe for pressure service), sch160, 20A. Two kinds of bolts with a diameter of 2.5 mm or 4 mm were used. As a result, the bolt 4 broke during testing. The breaking load in the case of a 2.5 mm bolt diameter was 20 KN, and the breaking load in the case of a 4 mm bolt diameter was 54 KN. The strength per unit cross-sectional area of the bolt 4 in the samples was 0.54 KN/mm² to

0.51 KN/mm², which are much the same. The tensile strength is calculated according to the cross-sectional area and the number of bolts 4.

Next, concerning the sample of FIG. 2, bolts 4 having a strength greater than the strength of the pressure pipes p1, p2 was used. The pressure pipes p1, p2 of this sample are made of STPG370 (carbon steel pipe for pressure service), sch80, 20A. The pressure pipes p1, p2, respectively, have a cross section of 285 mm², a tensile breaking load equal to or greater than 106 KN (105,450=370×285), and a yield load equal to or greater than the yield load of 62 KN. When four holes each having a diameter of 10 mm and a depth of 3.9 mm are used around the same circles, that is, along the same planes transverse to the longitudinal axis of the pressure pipes p1, p2, a decrease in the cross-sectional area of the pipes along the same circles of the pressure pipes p1, p2 becomes 156 mm² (10×3.9×4). The tensile breaking load of the base metal of the pressure pipes p1, p2 decreases from equal to or greater than 106 KN, which is in a state without a hole, to equal to or greater than 48 KN, because the cross-sectional area is decreased. Therefore, it is expected that the tensile breaking load of the base metal of the pressure pipes p1, p2 is below the yield load.

In a pulling test for this sample, the pressure pipes broke at a position along the circle on which bolt holes h1 are provided, at 78 KN. Therefore, it has been found that the pressure pipes of this case can withstand a tension bigger than the yield load. On the other hand, it is believed that the used pressure pipes made of STPG370 were stronger than the standardized strength of 370 N/mm² to begin with as a reason why the tension was bigger than the tensile breaking load calculated from the cross-sectional area of the pressure pipes p1, p2 of the sample of FIG. 2.

Furthermore, a sample of FIGS. 3A-3C is so formed that the pressure pipes are tightened with four bolts that are shifted in the length direction of the pressure pipes p1, p2 and by a 90 degrees angle on different circles, that is, different planes transverse to the length direction of the pressure pipes. In the sectional views, dashed-dotted lines show the holes that are formed on the cut pressure pipes. FIG. 3B is a perspective view of a sleeve 1, showing a situation in which bolt holes are provided on each of the circles a1, a2, a3 and a4, which are spaced from one another in the length direction of the pressure pipes. In the figures, chain double dashed lines show one of the circle passing through the center of each hole h1. In adjacent bolt holes, a shifting, or spacing, amount between the circles represents a distance between the closest outer diameters in a centerline c direction. In this sample, a shifting amount t is 2 mm. The shifting amount must be bigger than 0. FIG. 3C is a cross section showing a case where the bolts are screwed together. Each of the used bolts has a diameter of 10 mm and tensile strength of 1,000 N/mm².

In the case of this sample, the decrease in the cross-sectional area of the circles is 39 mm², which is equivalent to the dimensions of one lost hole. It is anticipated that the tensile breaking load of the base material of the pressure pipes p1, p2 on the circles a1, a2, a3 and a4 becomes equal to or greater than 92 KN, because the decrease in cross-sectional area reduces the strength. This value exceeds the yield load of 62 KN. On the other hand, when the sleeve 1 and the bolts have greater strength than the pressure pipes p1, p2, it is anticipated that a posterior position a5 of each of the holes h2 of the pressure pipes p1, p2 breaks due to the tension. When a tension test for each sample in FIGS. 3A-3C was performed, the pressure pipes broke at a load of 109 KN. A fracture surface continued obliquely from one hole to another. On the

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other hand, no breaks occurred at positions on the circles a1, a2, a3 and a4 of the pressure pipes p1, p2.

A pressure pipes of STPT410, sch160, 20A was tested for the sample shown in FIGS. 3A-3C in the same way. This pressure pipe has a cross-sectional area of 375 mm², a tensile breaking load equal to or greater than 154 KN, and a yield load equal to or greater than 92 KN. The expected tensile load of the base material of the pressure pipes p1, p2 at the positions of the circles a1, a2, a3 and a4 is 131 KN based on the cross-sectional area. The pressure pipe broke at a load of 134 KN in the test. A fracture surface obliquely continued from one hole to another, as in the previous test example. The bolt holes are arranged so as to be at equal angle intervals for all circles and not to overlap one another along a centerline direction. This is to equalize the shearing forces on the bolts.

The tests reveal that the cross-sectional area of the pressure pipes lost by the bolts can be reduced and yet the strength can be maintained by raising the tensile breaking load per unit area of the bolt. Here, because the shearing strength is expected to be 60% of the tensile strength, the strength of the bolt is 1.67 times (1/0.6) the tensile strength of the pressure pipe to be used. Therefore, it is desirable to use a bolt with strength equal to this.

Furthermore, although a sample in which adhesive was applied between the pressure pipes and the sleeve of FIGS. 3A-3C was, no improvement in the tensile strength was seen. however, it is expected that the use of the adhesive improves the sealing performance of the pressure pipes for air.

Moreover, the material of the sleeve has a tensile strength that is the same as, or greater than, the connected pressure pipes. Otherwise, a sleeve having a cross-sectional area that provides it with a tensile breaking load bigger than the tensile breaking load of the pressure pipes is used.

Thus, when the pressure pipes were connected with bolts, it was found that a tensile breaking load equal to or greater than the yield strength of the pressure pipes was shown without a break at least on the circles a1 to a4 of the pressure pipes having their cross-sectional area reduced by the bolts, due to proper control of the tensile shearing load, and the number and dispositions of the bolts.

Specifically, the bolts are arranged on the different circles, and the number of bolts and the strength of a bolt unit area can be determined for the yield strength of the pressure pipes and g as follows.

$$F < (S-L) \times N1 = n \times (\pi/2) \times 2 \times \pi \times N2 \times 0.6$$

Expression 1

In Expression 1, N1 is the tensile breaking strength of a pressure pipe per unit area; N2 is the tensile breaking strength of a bolt per unit area; r is the diameter of a bolt; S is the cross-sectional area of a pipe; n is the number of bolts; F is the yield load of a pressure pipe; L is the cross-sectional area lost due to a bolt hole on the same circle; and 0.6 is a correction factor for the strength of a bolt due to shearing force.

When there is a plurality of bolt holes on the same circle, the cross-sectional area L becomes the total cross-sectional area lost due to the bolts. Further, the cross-sectional area L becomes the cross-sectional area of the circle that is most greatly lost in case the cross-sectional area to be lost differs among the circles. The bolt hole may be provided to one place on the same circle because the strength of the pressure pipe is lost when a plurality of bolt holes are present on the same circle. Accordingly, it is possible to avoid breaks on the circles a1 to a4 and fracture of the bolts themselves when the cross-sectional area of the pressure pipe is reduced.

The following construction is used as a connecting structure of pipes for conveying a pressure fluid inside.

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The bolt holes do not penetrate the pressure pipes because inner fluid leaks outside through the bolt holes. In addition, sealing is performed at a position of an end face of the pressure pipes to limit the area with which the inner fluid comes in contact. Moreover, an O-ring is used, and a groove for the O-ring is provided, not on the end face of the pressure pipe but on an insert side, because the pressure pipe is often cut for length adjustment at a piping site, and it is difficult to notch the O-ring groove within the wall thickness of the pressure piping at the site. Hereinafter, concrete examples for connecting pressure pipes piping using a connection strength to be provided by a bolt will be explained with reference to the figures.

EXAMPLE 1

A connecting structure 100 related to a first example is illustrated in FIG. 4. The connecting structure 100 includes a sleeve 1a, an insert 2a, O-rings 3 and a plurality of bolts 4.

The sleeve 1a is a linear cylindrical pipe, and the insert 2a is inserted in an inner circumferential face side of the linear cylindrical pipe.

The insert 2a has annular faces b1, b2 in a centerline c direction of the sleeve 1a, and annular ring grooves b11, b21 are provided in the annular faces b1, b2, respectively. An O-ring 3 is put in each of the ring grooves b11, b21. The bolts 4 are tightened on different circles spaced in the centerline c direction, with each bolt 4 shifted 90 degrees from an adjacent bolt 4, as is the case with the connecting structure in FIG. 3. Holes h2 do not penetrate the pressure piping p1, p2 to prevent the inner fluid from leaking outside along a screw thread. The hole h1 of the sleeve 1a has no screw thread, but only the hole h2 has a screw thread. In accordance with this, the bolt 4 has a screw thread only at a position s that is to be screwed in the hole h2, but no screw thread between the position s and a head of the bolt 4. This is to improve the strength of the bolt. In place of the insert 2a, various sealants can be used as an insert depending on the fluid flowing in the pressure pipes p1, p2 (liquid, gas, low pressure, high pressure). For example, a gasket, packing and so on (FIG. 4C, 2c) can be used as a sealant to keep the connection airtight and watertight.

Referring now to a point to connect two pressure pipes p1, p2 having the connecting structure 100.

Ends of the pressure pipes p1, p2 are pushed into the sleeve 1a to the insert 2a from both sides and pressed toward each other to compress the O-ring 3 of the insert 2a. The compressed pressure is equivalent to prestress in using the O-ring 3.

Under this condition, the pressure pipes p1, p2 are marked in accordance with the position of a necessary plurality of holes h1. Then, the pressure pipes p1, p2 are removed from the sleeve 1a, and holes h2 are provided in the marked position. The depth of the hole h2 is not beyond the wall thickness of the pressure pipes p1, p2. A screw thread is provided in the holes h2.

Next, the pressure pipes p1, p2 are pushed into the sleeve 1a across from one another at the insert 2a and pressed by a pressure equivalent to the prestress of the O-ring 3 to return each of the pressure pipes p1, p2 and the sleeve 1a to the relative positions that had previously, positions corresponding to the positions for which the hole h2 was marked. Thereafter, the bolts 4 through the holes h1 of the sleeve 1a are screwed into the holes 2a and tightened, respectively. If a screw thread is simultaneously made in the holes h1, h2 when the pressure is applied from both sides on the pressure pipes p1, p2, the screw hole h2 can be made without marking, and screw threading bolts can be tightened in the holes h1, h2.

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In addition, if the ring grooves **b11**, **b21** have a depth just adapted for putting appropriate sealing pressure on the O-ring **3**, appropriate pressure is naturally put on the O-ring **3** by pushing the pressure pipe **p1** or **p2** into the sleeve **1a** or **1b** until the end face of the pressure pipe **p1** or **p2** contacts the annular face **b1** or **b2** of the insert **2a**. If the depths of the ring grooves **b11**, **b21** are decided in advance in this way, the locations of the holes **h2** can be identified and processed without marking, because it is known beforehand where along the pressure pipes **p1**, **p2** the holes **h1** of the sleeve **1a** or **1b** are located when the pipes **p1**, **p2** are pushed to their limits.

According to this, the pressure pipe **p1** is connected to the pressure pipe **p2** in the state that the appropriate prestress is imposed on the O-ring **3**. An adhesive can be used for the face of either the outer circumference area of the pressure pipes **p1**, **p2** or the inner circumferential face of the sleeve **1a** before again pushing the pressure pipes **p1**, **p2** into the sleeve **1a** after forming the hole **h2**. By using the adhesive, the fluid tightness is improved. The O-rings **3** are positioned at the end faces of the pressure pipes **p1**, **p2** because the insert **2a** is restricted from moving in the pipe by an inner wall of the sleeve **1a**. The areas of the perforated holes **h2** of the pressure pipes **p1**, **p2** are quenched by carburizing or induction quenching to increase the tensile strength for those areas, and to increase the tensile breaking load that was decreased by the forming of the perforated holes **h2** in the pressure pipes **p1**, **p2**.

In the first example, the pressure pipes **p1**, **p2** and the sleeve **1a** are made with steel materials, but use other metal materials.

EXAMPLE 2

FIG. 5 shows a connecting structure **101** related to a second example. In the connecting structure **101**, an annular neck portion **5** projects from the inner circumference of the sleeve **1b** at the center of the sleeve **1b**, in a lengthwise direction of the sleeve **1b**. Both side faces of the neck portion **5** are perpendicular to a centerline **c**, having the same radial dimension as the thickness of the pressure pipes **p1**, **p2**. In addition, the inner circumferential face of the neck portion **5** is a curved surface having the same diameter as the inner circumference of the pressure pipes **p1**, **p2**.

Inserts **2a** are respectively inserted from both ends of the sleeve **1b** with the O-rings **3**, and each comes into contact with the neck portion **5**. Even if all of the bolts **4** break, the sleeve **1b** can be restricted from slipping on the pressure pipes **p1**, **p2** and falling away from the contact portion because the neck portion **5** is provided.

Reference is made to a combination procedure for two pressure pipes **p1**, **p2** according to the connecting structure **101**. The insert **2a** is inserted from the sleeve **1b**, and then, the two pressure pipes **p1**, **p2** are pushed into the sleeve **1b** from both sides, and then, a pressing force is imposed on the pressure pipes **p1**, **p2**. The pressing force is equivalent to the prestress that the O-ring **3** mounted on the insert **2a** has in a use state.

Under this state, as in the case of the first example, the pressure pipes **p1**, **p2** are marked at positions corresponding to the positions of the holes **h1**, and thereafter, each of the pressure pipes **p1**, **p2** is pulled out of the sleeve **1b**, the holes **h2** are formed, and the screw thread is formed.

The inserts **2a** are respectively inserted from opposite ends of the sleeve **1b**, and the end portions of the pressure pipes **p1**, **p2** are pushed therein and tightened by screwing with bolts **4** while a pressing force corresponding to the prestress of the

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O-ring **3** is applied. In addition, an adhesive can be used between the pressure pipes **p1**, **p2** and the sleeve **1a** together with the bolts.

Just as in the earlier example, if the depth of the ring grooves **b11**, **b21** of the insert **2a** is made to such a depth that the O-ring **3** is fit for the ring grooves **b11**, **b21** when appropriate sealing pressure is applied thereon, the positions of the holes **h2** can be specified and processed without marking.

EXAMPLE 3

FIG. 6 shows a connecting structure **102** having a sleeve **1c** deformed relative to the sleeve **1b** of the second example and an insert **2b**. The area surrounding the neck portion **5** is deformed, and it is expanded and shown in the figure. In FIG. 6, each of the outer circumferential faces of a pair of inserts **2b** is formed into a conical male taper face whose diameter decreases in a direction toward the neck portion **5**, and each of a part of the inner circumferential faces of the sleeve **1c** is also formed in a conical male taper face whose diameter decreases in a direction toward the neck portion **5**.

According to this example, when each of the inserts **2b** is pushed toward the neck portion **5**, the sleeve **1c** and the pressure pipes **p1**, **p2** become concentrically positioned by the conical male taper face.

EXAMPLE 4

EXAMPLE 4 is explained with reference to FIG. 7. A connecting structure **103** of this example comprises a sleeve portion **1d**, a flange portion **6**, an insert **2a**, O-rings **3** and bolts **4**. In FIG. 7, generally the same reference characters are used as in EXAMPLE 2.

The sleeve portion **1d** and the flange portion **6** form a flange coupling **8** as a unified part. The flange portion **6** has an inner hole **6a** concentric with a hollow inside the sleeve portion **1d** as a fluid channel, besides having an annular face **6b** perpendicular to the centerline **c** between the inner hole **6a** and the sleeve portion **1d**. Multiple bolt holes **6c** are formed in an outer circumference portion of the flange portion **6** to insert bolts for connecting the flange portion **6** to a like flange coupling. The insert **2a** is inserted into the inner circumferential face of the sleeve portion **1d**. Here, multiple holes **h1** pass through the sleeve portion **1d**.

The order for connecting the pressure pipe **p1** according to the connecting structure **103** is the same as the order for connecting a pressure pipe at one side in EXAMPLE 2. The pressure pipe **p1** may be connected to the sleeve portion **1d** by using the annular face **6b**, just as the pipe **p1** is connected to the sleeve portion **1b** by using one of the sides of the neck portion **5** in EXAMPLE 2 (FIG. 5).

The thus connected pressure pipe **p1** with the flange portion **6** for example, bolts inserted into the bolt holes **6c** and nuts, and packing screwed on the bolts.

EXAMPLE 5

A connecting structure of EXAMPLE 5 may be so constructed that a female taper face having a diameter that decreases in a direction toward the annular face **6b** is formed on the inner circumferential face of the sleeve portion **1d** of EXAMPLE 4 and the insert **2b** of EXAMPLE 3. In this case, it is easy to locate the insert **2a**, as it is in EXAMPLE 3.

EXAMPLE 6

EXAMPLE 6 is explained with reference to FIG. 8. In a connecting structure **104** related to this example, a neck por-

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tion **5a** of a sleeve **1e** has annular ring-grooves **b11**, **b21** formed concentrically on the sides, respectively, unlike the neck portion **5** of the sleeve **1b** of EXAMPLE 2. Each of the ring-grooves **b11**, **b21** receives an O-ring **3**.

This structure is comparable to the neck portion **5** in EXAMPLE 2 with respect to the sealing function of the insert **2a**. In this example, it is not easy to install the O-rings **3** in the ring-grooves **b11**, **b21** formed in the inner part of the sleeve **1e**, but the number of parts can be reduced because the insert **2a** is not used.

EXAMPLE 7

The connecting structure **103** referred to EXAMPLE 4 can be transformed to a connecting structure **105** as shown in FIG. 9. In the connecting structure **105**, the tips of the outer circumferential faces of the pressure pipes **p1**, **p2** are respectively formed into tapering male faces. And the inner circumferential face of the sleeve **1f** is formed into a female tapering face toward the inner part.

Accordingly, even if there are radial gaps **g1**, **g2** between the inner circumferential face of the sleeve **1f** and the inserted pressure pipes **p1**, **p2**, they are automatically made concentric by the guiding of the male and female tapering faces.

EXAMPLE 8

FIG. 10 shows EXAMPLE 8. This is an example wherein the sleeve and the bolt are respectively modified. A bolt **4a** is a Phillips-screw, which has a screw thread on portion corresponding to the hole **h2** and notches **r** located at four portions positioned diagonally with respect to one another on the head. A bolt **4b** has a screw thread on the portion corresponding to the holes **h1**, **h2**. On the other hand, the hole **h1** of the sleeve **1g** has a square hollow **h3** on the outer circumferential side of the sleeve **1g**. FIG. 10B shows a detent **7**. The detent **7** has place surfaces corresponding to a spatial configuration that is formed between the square hollow and the circular bolt-head. A convex portion **7a** of the detent **7** is inserted into a notch **r** of the head of the bolt **4b**. The bolt **4a** is prevented from rotating by fitting the detents **7** into the four spaces between the hollow **h3** and the head of the bolt **4a**. The detent **7** may be made out of stainless steel.

EXAMPLE 9

FIG. 11 shows EXAMPLE 9. This example refers to a flange coupling **11**, which is the same as having changed a part of the flange coupling **8** in the connecting structure **103** of EXAMPLE 4, and generally the reference characters of EXAMPLE 4 are used in EXAMPLE 9.

A sleeve **1h** and a flange portion **9** form a unified part. The flange portion **9** has an inner hole **9a** as a fluid channel. The flange coupling **11** differs from the flange coupling **8** of EXAMPLE 4 in that the flange portion **6** and the sleeve portion **1d** are continuously connected without a perpendicular annular face **6b** (FIG. 7) therebetween. Therefore, the pressure pipe **p1** has an end face that reaches an end face **9b** of the flange portion **9** through a hollow of the flange coupling **11**. The end portion of the pressure piping **p1** can either pass through the flange coupling **11** and protrude from the end face **9b** or stop short before the end face **9b**. The multiple bolt holes **6c** for inserting the bolts are formed on an outer circumferential portion of the flange portion **6**. As shown in FIG. 11B, in the case of connecting to another flange coupling after connecting to the pressure pipe **p1**, the insert **2a** and the packing **10** (FIG. 11) are supplied on the end face of the

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pressure pipe **p1** or both the end face of the pressure pipe **p1** and the end face **9b** of the flange portion **9**. Here, the end face of the pressure pipe **p1** is exposed, and therefore, seals such as the insert **2a** and the packing **10** can be immediately dropped out when removing the flange coupling **11** from the other coupling.

EXAMPLE 10

FIG. 12 shows EXAMPLE 10. This example refers to a flange coupling **12**, which is the same as having changed a part of flange coupling **8** in the connecting structure **103** of EXAMPLE 4, and generally the same reference characters are used in EXAMPLE 10 and EXAMPLE 4. A flange portion **12a**, which has a bolt hole **12b** for connecting with the other flange coupling, overlaps with a sleeve portion **12c**. The hole **h1** provided in the sleeve portion **12c** and the bolt hole **12b** are shifted relative to one another so as not to interfere with one another. The flange coupling **12** can be considered to have the outer circumferential face of the flange portion **6** of EXAMPLE 4 just continued to the sleeve portion **1d** (FIG. 7).

EXAMPLE 11

FIG. 13 shows EXAMPLE 11. This example refers to a flange coupling **14** having a flange portion on the pressure pipe **p1** of EXAMPLE 1. A connection with the pressure pipe **p2** conforms to EXAMPLE 1.

EXAMPLE 12

In FIG. 14, an insert **2a** or a sheet packing **2d** can be used with the flange coupling **12** in EXAMPLE 12 in order to connect to the other flange coupling.

EXAMPLE 13

The bolt **4** connecting the pressure pipes **p1**, **p2** to the sleeve bears shear force at the contact surface between the sleeve and the pressure pipe. FIG. 15 shows a bolt **40** whose shear strength is great. A shank portion **40a** of the bolt **40**, which is located in the contact surface **PL**, forms a straight curved surface without a screw thread.

EXAMPLE 14

In addition, the connecting structure may be constructed so that an insert can be connected to the sleeve with bolts. In FIG. 16, an insert **2e** is formed into a pipe having the same inside diameter as the pressure pipes **p1**, **p2**, and blind threaded holes **h4** on its outer surface. The sleeve **1a** has through holes **h5** at positions corresponding to the threaded holes **h4** (which can have screw threads), and the insert **2e** is connected to the sleeve **1a** with the bolts **4**.

In this structure, when removing the pressure pipe **p2**, all bolts **4** are removed, and the end of the pressure pipe **p2** is exposed by sliding the sleeve **1a** to the left. Therefore, the pressure pipe **p2** can be removed without changing the positional relationship of the pressure pipe **p1** installed in the spot.

EXAMPLE 15

FIG. 17 shows the other example for connecting pressure piping with a loose coupling. In FIG. 17C, a cylindrical sleeve **1i** has multiple through holes **h1** provided at separate locations in the lengthwise direction, and at equiangular intervals with respect to one another and without overlapping in the

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circumferential direction, as is also true of the sleeve 1a and so on of the former examples. However, the sleeve 1i extends to the end of the pressure piping p2. On the other hand, a loose coupling 13 is used to connect the pressure pipe p2 with another pipe. The loose coupling 13 has a flange portion 13a contacting one end e of the sleeve 1i, a body portion 13b extending to the other end f of the sleeve 1i at the outer surface of the sleeve 1i, and bolt holes 13c for connecting the loose coupling 13 with another loose coupling. In the present invention, although the body portion 13b has a length extending to the other end f of the sleeve 1i, it does not have to extend thereto.

During assembly connecting structure of the, the pressure pipe p2 is put through the loose coupling 13 as shown in FIG. 17A, and then, the sleeve 1i is secured on the pressure piping p2 with bolts 4 as shown in FIG. 17B (in the figure, the bolts 4b are shown). As for the bolts 4, a bolt whose head does not protrude from the outer surface of the sleeve 1i is used. The bolts 4b may be used with the detents 7 of FIG. 10B. The pressure pipe p2 has non-through threaded holes h2 at locations corresponding to the holes h1, as in the former example. Likewise, the sleeve 1i is fixed on the pressure pipe p1 with the bolts 4b, and the couplings are fixed with a bolt m and a nut n. Various inserts for sealing as shown with arrows in FIG. 17C (such as a gasket, a packing, an O-ring and so on) are put between the pressure pipe p1 and the pressure pipe p2. The end surface of the pressure pipe p2 (or the pressure pipe p1) may act as a sealing face on which a seal is located, and therefore, the seal may be located on the end surface of the sleeve 1i or the loose coupling, or not. The partner coupling connecting with the loose coupling may be a flange coupling such as that of FIG. 7 or FIG. 12, or another form.

EXAMPLE 16

FIG. 18 shows an example, in which specified prestress is given to the insert 2a for sealing by screwing the pressure pipe p1 (or p2) in the sleeves 1a, 1b. FIG. 18A shows an embodiment of FIG. 4A (EXAMPLE 1); FIG. 18B shows an embodiment of FIG. 5A (EXAMPLE 2); and FIG. 18C shows an embodiment of FIG. 16 (EXAMPLE 16), each as an example, respectively. Screw threads sc1 are provided on the outer circumference of the pressure pipe p1, p2, respectively, and screw threads sc2 for cooperating with the screw threads sc1 are provided on the inner circumference of the sleeves 1a, 1b, respectively. The inserts 2a, 2e have pressure applied to them by screwing the pressure pipe p1 or the pressure pipe p2 into the sleeve 1a or the sleeve 1b.

The prestress on the sealing material of the inserts 2a, 2e can be determined by adjusting the screwed length. The present invention can be applied to the case in which the sleeve portions 1d, 12c of the flange portions disclosed in the embodiments of FIG. 7 (EXAMPLE 4) and the embodiment of FIG. 12 (EXAMPLE 10) are connected with the pressure pipe p1 through the insert 2a.

If the insert 2a has the ring grooves b11, b21 with a depth to fit the O-ring when proper sealing pressure is applied thereto, proper pressure comes to be spontaneously added on the O-ring by screwing the pressure pipe p1 or the pressure pipe p2 into the sleeve 1a or the sleeve 1b until the end face thereof contacts the annular faces b1, b2 of the insert 2a.

EXAMPLE 17

In EXAMPLE 8 shown in FIG. 10, the bolt 4a has the screw thread on only a portion corresponding to the hole h2, but the portion may be formed columnar and the screw thread may be provided on only a portion corresponding to the hole h1. In FIG. 19, a bolt 4c has a screw thread on a portion s1 corre-

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sponding to the hole h1, and a portion s2 corresponding to the hole h2 is columnar, without a screw thread. The pressure pipes p1, p2 have no screw threads on the holes h2, and each hole h2 is a cylindrical non-through hole for inserting the columnar portion s2 of the bolt 4c. On the other hand, the sleeve 1a is the same as the sleeve shown in FIG. 4. Further, the pressure pipes p1, p2 have the insert 2a shown in the embodiment of FIG. 4 inserted therebetween. The O-ring 3 in the insert 2a can seal with necessary proper pressure by inserting the portion s2 of the bolt 4c into the hole h2 after locating the insert between the pressure pipe p1 and the pressure pipe p2 under compression. According to the present embodiment, the hole h2 has an inner surface formed as a smooth column curved surface, and therefore, the pressure pipe has high strength. The features shown above can be applied to all EXAMPLES 1 to 16.

EXAMPLE 18

FIG. 20A shows an example for using the bolts 4c of FIG. 19 and connecting the pressure pipes p1, p2 through the insert 2e (FIG. 16). In the present example, the insert 2e is fixed on the sleeve 1a, and thereafter, the portion s2 of the bolt 4c is inserted into the hole h2 in the situation where the O-rings on left and right sides of insert 2e are compressed with proper pressure by respectively pushing the pressure pipes p1, p2 into the sleeve 1a.

EXAMPLE 19

FIG. 20C shows an insert 2f reformed for a thick O-ring. FIG. 20B shows the situation in which the pressure pipes p1, p2 are connected through the insert 2f.

The insert 2f is a form of ring; its inner circumferential surface 20 has a diameter that is the same as the internal circumferential surface of the pressure pipes p1; and its outer circumferential surface 21 has a diameter slightly smaller than the outer circumferential surface of the sleeve 1a. There are step-shaped grooves 23 in a concentric circle form in the outer circumferential surface 21 of the insert 2f at the right and left end faces 22 thereof. The step-shaped groove 23 has an annular face 24 parallel to the radial direction and a ring face 25 parallel to the centerline.

Besides, in the insert 2f, if the ring face 25 has a width such that the O-ring 3 just achieves the height of the end face 22 when proper sealing pressure is added on the O-ring 3, the proper pressure is spontaneously added to the O-ring 3 by pushing the pressure pipe p1 or the pressure pipe p2 into the sleeve 1a or the sleeve 1b until its end face hits the end face 22.

The insert 2f has non-through holes 26 that are used to fix to the sleeve 1a. The sleeve 1a has holes 5 passing from the outer circumferential surface to the inner circumferential surface. The holes 5 are connected to the holes 26 of the insert 2f with the bolts 4.

When fixing the insert 2f to the sleeve 1a with the bolts 4, the inner circumferential surfaces of the annular face 24, the ring face 25 and the sleeve 1a form the bottom face and both side faces of the groove for the O-ring 3, respectively.

A thick O-ring is superior in stabilizing seal characteristics, because it has a small compression set compressibility is constant. According to the present example, it is possible to use the thick O-ring. In addition, the bolts 4c were used, because the pressure pipes p1, p2 have no screw threads in the holes. However, the holes h2 may have screw threads, and in that case, the bolts 4 are used.

Furthermore, in the insert 2f, if the ring face 25 has a width such that the O-ring just achieves in the width of the ring face when the proper seal pressure is imposed on the O-ring 3, the proper pressure is spontaneously imposed on the O-ring 3 by

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pushing the pressure pipe p1 or p2 into the sleeve 1a or 1b until its end face hits the end face 22.

EXAMPLE 20

FIG. 21A shows an embodiment in which an insert 2g (FIG. 21B) is adapted to the connecting structure 103 of EXAMPLE 4 (FIG. 7). The insert 2g is formed as a ring as the insert 2f; its inner circumferential surface 20 has the same diameter as the inner circumferential surface of the pressure pipe p1; and its outer circumferential surface 21 has a diameter smaller than the inner circumferential surface of the sleeve 1d to some extent. A concentrically hollow step-shaped groove 23 is provided in the outer circumferential surface 21 at each of the end faces 22. The step-shaped groove 23 has an annular face 24 parallel to the radial direction and a ring face 25 parallel to the centerline. The insert 2g has no non-through holes 26, such as those shown in the insert 2f. The insert 2g does not need to be fixed, because it is sandwiched between the neck portion 6b and the pressure pipe p1. The holes h2 of the pressure pipes p1, p2 may have screw threads. In that case, the bolts 4 are used.

EXAMPLE 21

FIG. 21C shows a modification of the connecting structure 101 of EXAMPLE 2 in FIG. 5. In FIG. 21C, a screw thread is provided in the hole h1 of the sleeve 1b, and not provided in the holes h2 of the pressure pipes p1, p2, respectively. A ring-shaped neck portion 5 protrudes from the inner circumferential surface of the sleeve 1b, and the insert 2g is placed against the neck portion. The sleeve 1b is connected to the pressure pipes p1, p2 by the bolts 4c (FIG. 19). The O-ring of the insert 2g is compressed as mentioned previously. Since the holes h2 have no screw threads, the bolts 4c are used. However, the holes h2 may have screw threads. In that case, the bolts 4 are used.

EXAMPLE 22

FIG. 22 shows a modification of EXAMPLE 16 in FIG. 18. In this embodiment, the O-ring 3 is compressed by screwing the pressure pipe p1 (or p2) into the sleeve to the insert 2f or 2g, which seals as in FIG. 16. Screw threads sc2 are provided along the full length of the inner circumferential surfaces of the sleeve 1a, 1b including the portion of the hole h1. On the other hand, screw threads sc1 that screw together with the screw threads sc2 are provided on the outer circumferential surfaces of the pressure pipes p1, p2. Pressure is put on the insert 2f or 2g by screwing the pressure pipe p1 or p2 into the sleeve 1a or 1b. Prestress is added to the O-ring by adjusting the amount of engagement.

In making the ring face 25 of the insert 2g to have such a width that the O-ring 3 fits in completely with proper seal pressure, the proper pressure is spontaneously imposed on the O-ring 3 by pushing the pressure pipe p1 or p2 into the sleeve 1a or 1b until its end face engages the end face 22 of the insert 2g. Since screw threads are not formed in the holes 2 of the pressure pipes p1, p2, the bolts 4c are used. However, the holes h2 may have screw threads. In that case, the bolts 4 are used.

EXPLANATION OF REFERENCED NUMERALS

100 to 105 connecting structure
1, 1a to 1i sleeve or sleeve portion
2 insert

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3 O-ring
4, 4a bolt
5 neck portion
6 flange portion
7 detent
8 flange coupling
p1 pressure pipe
p2 pressure pipe

The invention claimed is:

1. A pressure piping assembly in which pressurized fluid flows, said pressure piping assembly comprising:

a cylindrical sleeve having a plurality of through holes, said through holes being provided at separate locations in a lengthwise direction and with identical angular intervals in a circumferential direction and without overlapping in the circumferential direction, said cylindrical sleeve having an interior space for receiving pressure piping and wherein a sum of the identical angular intervals between the plurality of through holes is 360 degrees;

a plurality of bolts for being inserted into the holes of the sleeve; and,

at least one pressure pipe having non-through holes being positioned at locations corresponding to the holes of the sleeve, whereby, when the at least one pressure pipe is inserted into the interior space of the sleeve, the non-through holes of the at least one pressure pipe communicate with the respective holes of the sleeve, and said bolts are inserted through the holes extending through the sleeve into the non-through holes.

2. A pressure piping assembly as claimed in claim 1, wherein the non-through holes each having a cylindrical smooth inner circumferential surface, each of said bolts has a portion without a screw thread to be inserted into the non-through hole, and when the at least one pressure pipe is inserted into the interior space of the sleeve, the at least one pressure pipe aligns with the sleeve such that the holes of the at least one pressure pipe communicate with corresponding holes of the sleeve.

3. A pressure piping assembly for conveying pressurized fluid, said pressure piping assembly comprising:

a cylindrical sleeve having a first end, a second end and a first set of through holes, said first set of through holes being provided at separate locations in a lengthwise direction and with identical angular intervals in a circumferential direction and without overlapping in the circumferential direction, said cylindrical sleeve having a first pressure pipe inserted into an interior of cylindrical sleeve from said first end and a second pressure pipe inserted into the interior from said second end and wherein a sum of the identical angular intervals between the first set of through holes is 360 degrees;

an insert for sealing the pressure pipes, said insert being located in the interior of the sleeve, sandwiched between the pressure pipes; and

a plurality of bolts for being inserted into the holes of the sleeve,

wherein said pressure pipes have a first set of non-through holes at locations corresponding to the holes of the sleeve, and wherein, when the pressure pipes are inserted into the interior of the sleeve, each non-through hole of the first set of non-through holes communicates with a corresponding through hole of the first set of through holes, and said bolts are screwed on the screw threads of holes in one of the first set of through holes and the first set of non-through holes.

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